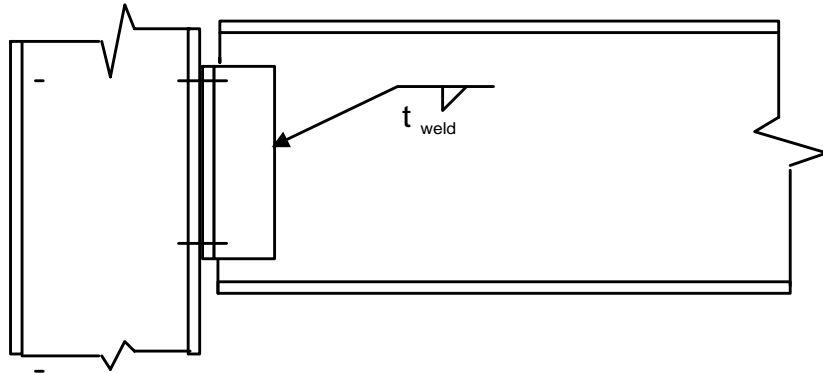


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SIMPLE BEAM TO COLUMN CONNECTION

CONNECTION TYPE:BEAM TO COLUMN/CLIP ANGLE/BOLTED AT COLUMN

CONNECTION TYPE :BC-5/20/734 + AXIAL=50 kN



Description:

- 2 clip angles welded to flange of beam
- 2 clip angles bolted to flange or web of column

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FOR DIMENSIONS AND CAPACITY SEE THE LAST PAGE  
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**INPUT DATA**  
-----**COLUMN:**  $F_{yg} := 300 \cdot \text{MPa}$   $F_{ug} := 450 \cdot \text{MPa}$ **BEAM :** $F_{yb} := 300 \cdot \text{MPa}$  $F_{ub} := 450 \cdot \text{MPa}$  $db := 460 \cdot \text{mm}$   $Bb := 191 \cdot \text{mm}$   $t_{fb} := 16 \cdot \text{mm}$   $twb := 9.9 \cdot \text{mm}$ **CLIP ANGLE :** $LEG := 100 \cdot \text{mm}$   $ta := 12 \cdot \text{mm}$   $F_{ya} := 235 \cdot \text{MPa}$   $F_{ua} := 375 \cdot \text{MPa}$ **Clip Angle Length :**  $l := 400 \cdot \text{mm}$ **Clip Angle Weld to Beam:**  $t_{weld} := 10 \cdot \text{mm}$ **BOLT : ASTM A325 Class B Surface** $N := 5$  **number of rows of bolts** $d := 20 \cdot \text{mm}$   $F_{ubolt} := 830 \cdot \text{MPa}$  $V_s := 0.53 \cdot 0.50 \cdot 0.89 \cdot \pi \cdot \frac{d^2}{4} \cdot F_{ubolt}$   $T_r := 0.75 \cdot 0.67 \cdot \pi \cdot \frac{d^2}{4} \cdot F_{ubolt}$  $V_s = 61.5 \text{ kN}$  $T_r = 131 \text{ kN}$ **PITCH**  $p := 80 \cdot \text{mm}$  **EDGE DISTANCE**  $e := 40 \cdot \text{mm}$  **GAGE**  $G := 120 \cdot \text{mm}$ **TOS to 1st bolt**  $d_p := 100 \cdot \text{mm}$ **AXIAL LOAD:**  $P_f := 50 \cdot \text{kN}$ **WELD :**  $X_u := 480 \cdot \text{MPa}$ **RESISTANCE FACTORS :**  $\phi := 0.9$   $\phi_w := 0.67$ **REFERENCES:** 1) CAN/CSA-S16.1-94 LIMIT STATES DESIGN OF STEEL STRUCTURES  
2) AMERICAN INSTITUTE OF STEEL CONSTRUCTION:MANUAL OF STEEL CONSTRUCTION/VOLUME II/CONNECTIONS**1.0 CALCULATION OF SHEAR CAPACITY OF BOLTS****1.1 CHECK BOLT SHEAR CAPACITY FOR SERVICE LOAD** $V_{bolt} := 2 \cdot N \cdot V_s$   $V_{bolt} = 614.98 \text{ kN}$ **2.0 CHECK WEB SHEAR CAPACITY****2.1 WEB SHEAR CHECK** $h := db$  $V_{rs} := \phi \cdot 0.5 \cdot twb \cdot h \cdot F_{ub}$   $V_{rs} = 922.2 \text{ kN}$ **2.2 WEB BLOCK SHEAR CHECK**

$$t_{wb} = 9.9 \text{ mm}$$

$$V_{bs} := \phi \cdot \left[ 0.5 \cdot l + \frac{0.85 \cdot (\text{LEG} - 10 \cdot \text{mm})}{2} \right] \cdot t_{wb} \cdot F_{ub}$$

$$V_{bs} = 955.3 \text{ kN}$$

### 3.0 CHECK CLIP ANGLE CAPACITY

#### 3.1 SHEAR CHECK OF CLIP ANGLE

$$L_n := l - N \cdot (d + 4 \cdot \text{mm}) \quad L_n = 280 \text{ mm}$$

$$V_r := (0.5 \cdot \phi \cdot L_n \cdot t_a \cdot F_{ua}) \cdot 2 \quad V_r = 1134 \text{ kN}$$

#### 3.2 BOLT CAPACITY BY BEARING

$$Br_1 := 0.67 \cdot t_a \cdot e \cdot F_{ua} \quad Br_2 := 3 \cdot 0.67 \cdot t_a \cdot d \cdot F_{ua}$$

$$Br_3 := 0.67 \cdot 0.7 \cdot \pi \cdot \frac{d^2}{4} \cdot 0.6 \cdot F_{ubolt}$$

$$Br := \min \left( \begin{array}{l} (Br_1) \\ (Br_2) \\ (Br_3) \end{array} \right) \quad Br = 73.4 \text{ kN}$$

$$V_{bolt_{bear}} := 2 \cdot N \cdot Br \quad V_{bolt_{bear}} = 733.76 \text{ kN}$$

### 4.0 MAXIMUM CAPACITY OF CONNECTION

$$V_{estim} := 750 \cdot \text{kN}$$

To control weld size in Section 6.3, cope length and web thickness of supporting girder and axial force

$$V_{MAX} := \min \left( \begin{array}{l} (V_{rs}) \\ (V_{bs}) \\ (V_r) \\ (V_{bolt_{bear}}) \\ (V_{estim}) \end{array} \right) \quad V_{MAX} = 733.76 \text{ kN} < 1.33 \cdot V_{bolt} = 817.93 \text{ kN}$$

### 5.0 CHECK MINIMUM PLATE GIRDER THICKNESS (assuming one beam on each side)

$$t_{wg} := \frac{V_{MAX}}{3 \cdot 0.67 \cdot d \cdot F_{ug} \cdot 2 \cdot N} \quad t_{wg} = 4.06 \text{ mm}$$

### 6.0 CHECK BEAM TO CLIP ANGLE WELD

#### 6.1 WELD TREATED AS A LINE (INCLUDING EFFECT OF AXIAL FORCE)

$$k_1 := \text{LEG} - 10 \cdot \text{mm} \quad x_1 := \frac{k_1^2}{2 \cdot k_1 + 1} \quad a_1 := \text{LEG} - x_1$$

$$I_p := \frac{k_1^3}{3} \cdot \frac{k_1 + 2 \cdot l}{1 + 2 \cdot k_1} + \frac{l^2}{12} \cdot (6 \cdot k_1 + 1)$$

$$f_h := \frac{0.5 \cdot V_{MAX} \cdot a_1 \cdot l}{2 \cdot I_p} + \frac{0.5 \cdot P_f}{2 \cdot k_l + l}$$

$$f_v := \frac{0.5 \cdot V_{MAX}}{2 \cdot k_l + l} + \frac{0.5 \cdot V_{MAX} \cdot a_1 \cdot (k_l - x_l)}{I_p}$$

$$f_r := \sqrt{f_h^2 + f_v^2} \qquad f_r = 0.98 \frac{\text{kN}}{\text{mm}}$$

**6.2 FACTORED FILLET WELD CAPACITY :**

$$F_y := \text{if}(F_{ya} > F_{yb}, F_{yb}, F_{ya})$$

$$V_{r1} := 0.67 \cdot \phi \cdot F_y \qquad V_{r2} := 0.67 \cdot \phi_w \cdot 0.707 \cdot X_u$$

$$V_r := \text{if}(V_{r1} > V_{r2}, V_{r2}, V_{r1})$$

$$V_r = 0.14 \frac{\text{kN}}{\text{mm}^2}$$

**6.3 REQUIRED WELD SIZE :**

$$t_{w_{reqd}} := \frac{f_r}{V_r} \qquad t_{w_{reqd}} = 6.9 \text{ mm}$$

$$< t_{w_{eld}} = 10 \text{ mm}$$

**6.4 CHECK WEB STRESS IN BEAM WEB:**

$$t_{wb} = 9.9 \text{ mm}$$

$$F_r := 0.67 \cdot \phi \cdot F_{yb} \cdot t_{wb}$$

$$F_r = 1.79 \frac{\text{kN}}{\text{mm}} \geq f_r = 0.98 \frac{\text{kN}}{\text{mm}}$$

**7.0 AXIAL LOAD CAPACITY**

$$P_f = 50 \text{ kN}$$

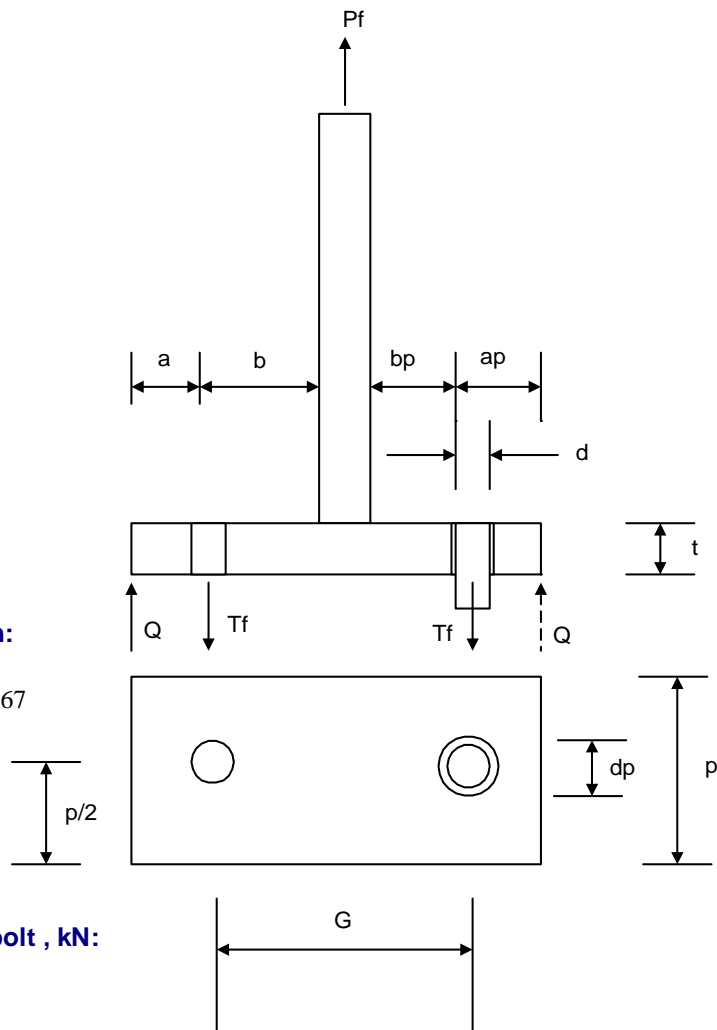
**7.1 Prying Action**

**Total applied factored force:**

$$P_f = 50 \text{ kN}$$

**Number of flange bolts in tension:**

$$n := 2 \cdot N \qquad n = 10 \qquad \phi_b := 0.67$$



**Applied factored tensile load per bolt , kN:**

$$P_{fb} := \frac{P_f}{n} \qquad P_{fb} = 5 \text{ kN}$$

**Factored tensile resistance of bolts, kN:**

$$T_r := \phi_b \cdot 0.75 \cdot \pi \cdot \frac{d^2}{4} \cdot F_{ubolt} \quad T_r = 131.03 \text{ kN}$$

**Yield strength of plate material:**  $F_{ya} = 235 \text{ MPa}$

$$a := e \quad a = 40 \text{ mm}$$

$$a_p := a + \frac{d}{2} \quad a_p = 50 \text{ mm} \quad d_p := d + 4 \cdot \text{mm} \quad d_p = 24 \text{ mm}$$

$$p = 80 \text{ mm} \quad t_a = 12 \text{ mm} \quad \phi = 0.9$$

$$b_p := \text{LEG} - t_a - a_p \quad b_p = 38 \text{ mm}$$

$$\delta := \frac{[p - (d + 2 \cdot \text{mm})] \cdot t_a}{p \cdot t_a} \quad \delta = 0.73$$

$$\alpha := \frac{1}{\delta} \cdot \left( \frac{4 \cdot P_{fb} \cdot b_p}{\phi \cdot p \cdot t_a^2 \cdot F_{ya}} - 1 \right) \quad \alpha := \text{if} \left[ \alpha > 1, 1, \max \left( \left( \begin{array}{c} \alpha \\ 0 \end{array} \right) \right) \right] \quad \alpha = 0$$

**Prying force:**  $Q := P_{fb} \cdot \frac{\alpha \cdot \delta}{1 + \alpha \cdot \delta} \cdot \frac{b_p}{a_p} \quad Q = 0 \text{ kN}$

**Total force in bolts:**  $T_f := P_{fb} + Q$

$$T_f = 5 \text{ kN} < T_r = 131.03 \text{ kN}$$

## 8.2 CHECK BOLTS IN COMBINED SHEAR AND TENSION

### FOR BEARING:

$$\left( \frac{V_{MAX}}{V_{bolt_{bear}}} \right)^2 + \left( \frac{P_{fb}}{T_r} \right)^2 = 1 \quad \leq 1.0$$

### FOR SLIP CRITICAL

$$\frac{\frac{V_{MAX}}{1.33}}{V_{bolt}} + \frac{1.9 \cdot \frac{P_{fb}}{1.33}}{\frac{d^2}{n \cdot \pi \cdot \frac{d^2}{4}} \cdot F_{ubolt}} = 0.9 < 1.0$$

## 8.3 CHECK PLATE THICKNESS REQUIRED FOR BENDING DUE TO AXIAL FORCE

$$M_{fa} := \frac{P_{fb} \cdot b_p}{(1 + \alpha \cdot \delta)} \quad M_{fa} = 0.19 \text{ kN} \cdot \text{m}$$

$$t_{required} := \sqrt{\frac{4 \cdot M_{fa}}{\phi \cdot F_{ya} \cdot p}}$$

$$t_{required} = 6.7 \text{ mm} \leq t_a = 12 \text{ mm}$$

$$M_r := \phi \cdot p \cdot \frac{t_{required}^2}{4} \cdot F_{ya} \quad M_r = 0.19 \text{ kN} \cdot \text{m}$$

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SUMMARY - CONNECTION TYPE PARAMETERS  
-----Bolts

Minimum number of bolts rows	$N = 5$
Minimum number of bolts	$2 \cdot N = 10$
Minimum bolt diameter	$d = 20 \text{ mm}$
Maximum bolt pitch	$p = 80 \text{ mm}$
Bolt Gauge at girder	$G = 120 \text{ mm}$
Minimum edge distance	$e = 40 \text{ mm}$

Beam characteristics

Minimum steel yield strength	$F_{yb} = 300 \text{ MPa}$
Maximum beam depth	$d_b = 460 \text{ mm}$
Minimum flange width	$B_b = 191 \text{ mm}$
Minimum flange thickness	$t_{fb} = 16 \text{ mm}$
Minimum web thickness	$t_{wb} = 9.9 \text{ mm}$
Minimum distance from Top of Steel (TOS) to first row of bolts	$d_p = 100 \text{ mm}$

Column Characteristics

Minimum steel yield strength	$F_{yg} = 300 \text{ MPa}$
Minimum flange or web thickness	$t_{wg} = 4.06 \text{ mm}$

Clip Angle Characteristics

Minimum Length	$l = 400 \text{ mm}$
Minimum steel yield strength	$F_{ya} = 235 \text{ MPa}$
Minimum leg dimension	$LEG = 100 \text{ mm}$
Minimum thickness	$t_a = 12 \text{ mm}$

Weld Characteristics

Fillet weld size	$t_{weld} = 10 \text{ mm}$
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<u>Maximum Axial Force</u>	$P_f = 50 \text{ kN}$
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CAPACITY OF CONNECTION

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 $V_{MAX} = 733.76 \text{ kN}$   
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